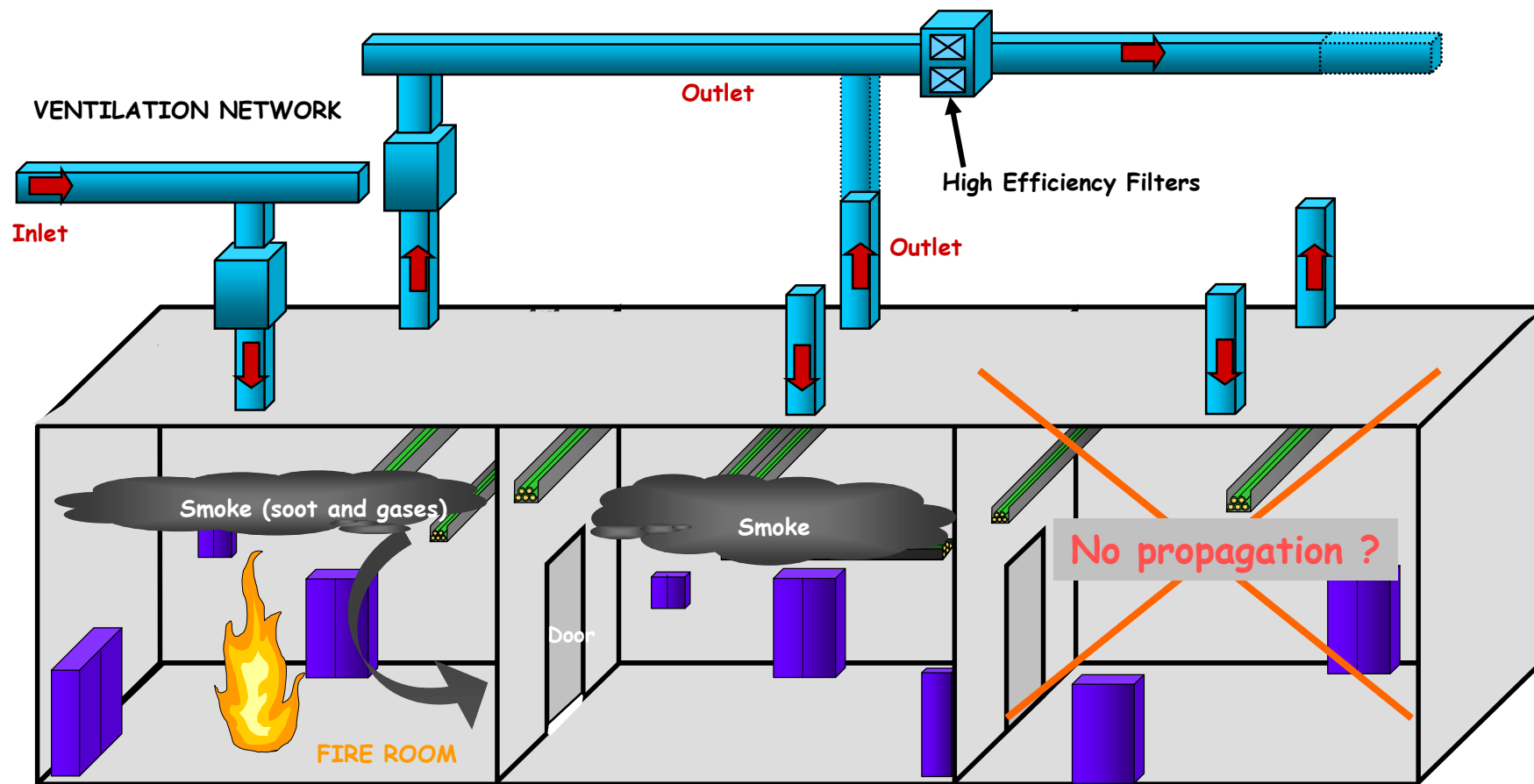


Contents

- **Context**
- **Overview of the PRISME Program**
- **Overview of the PRISME benchmarking Group**

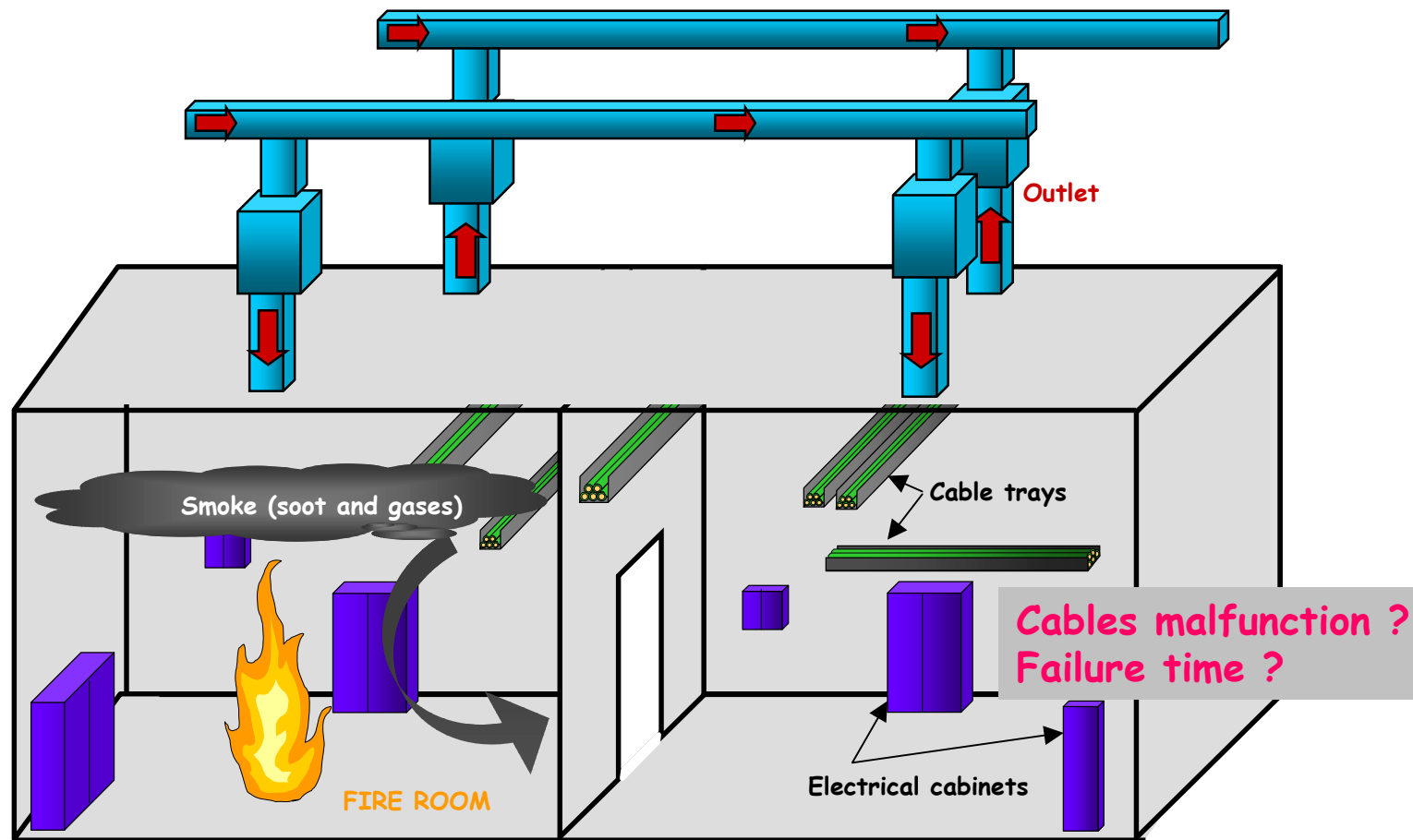
Fire Safety assumptions/questions

- Propagation of heat and smoke from the fire room towards others rooms



Fire Safety assumptions/questions

- Impact of heat and smoke on safety critical systems



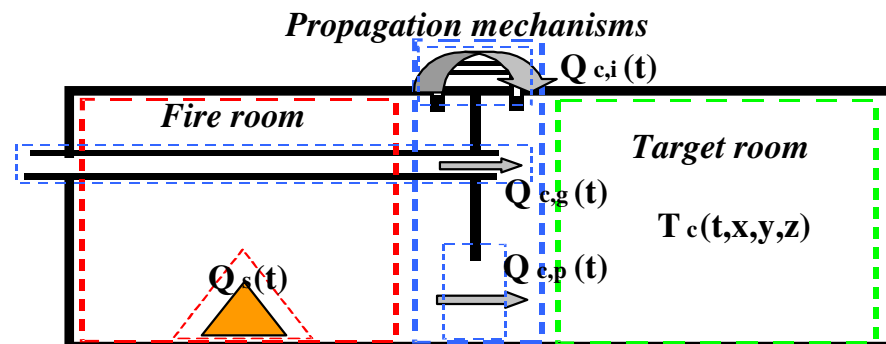
OECD PRISME Program (2006-2010)

■ Partners:

- Belgium (AVN, Tractebel), Canada (AECL), Finland (VTT, STUK), France (IRSN, EDF, DGA [IUSTI]), Germany (GRS, iBMB), Japan (JNES), Netherlands (NRG), Spain (CSN), Sweden (Ringhals AB), Korean (KINS), UK (HSE), USA (NRC)

■ Objectives:

- Primary objectives of the project:
 - To study the mechanism of smoke and heat propagation from a fire within a room towards neighbouring rooms in a confined and mechanically ventilated facility
- Secondary objectives of the project:
 - To study equipment behaviour when submitted to thermal stresses generated by a fire: for instance electrical cables failure and degradation

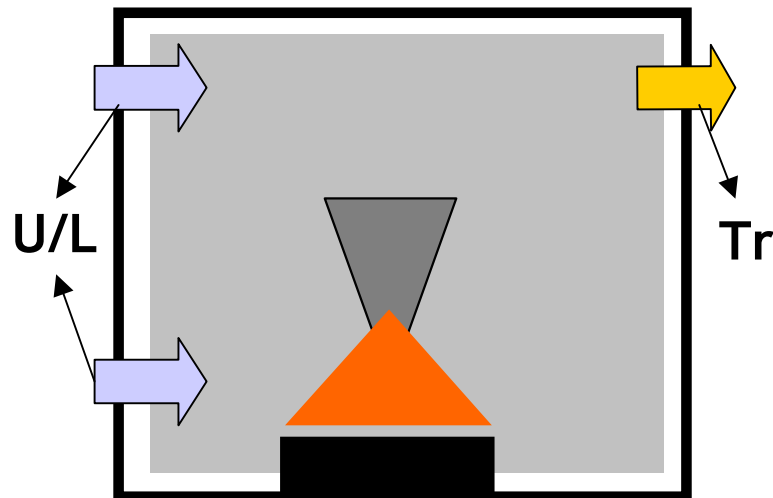


PRISME Program (2006-2010)

■ Fire source characterization

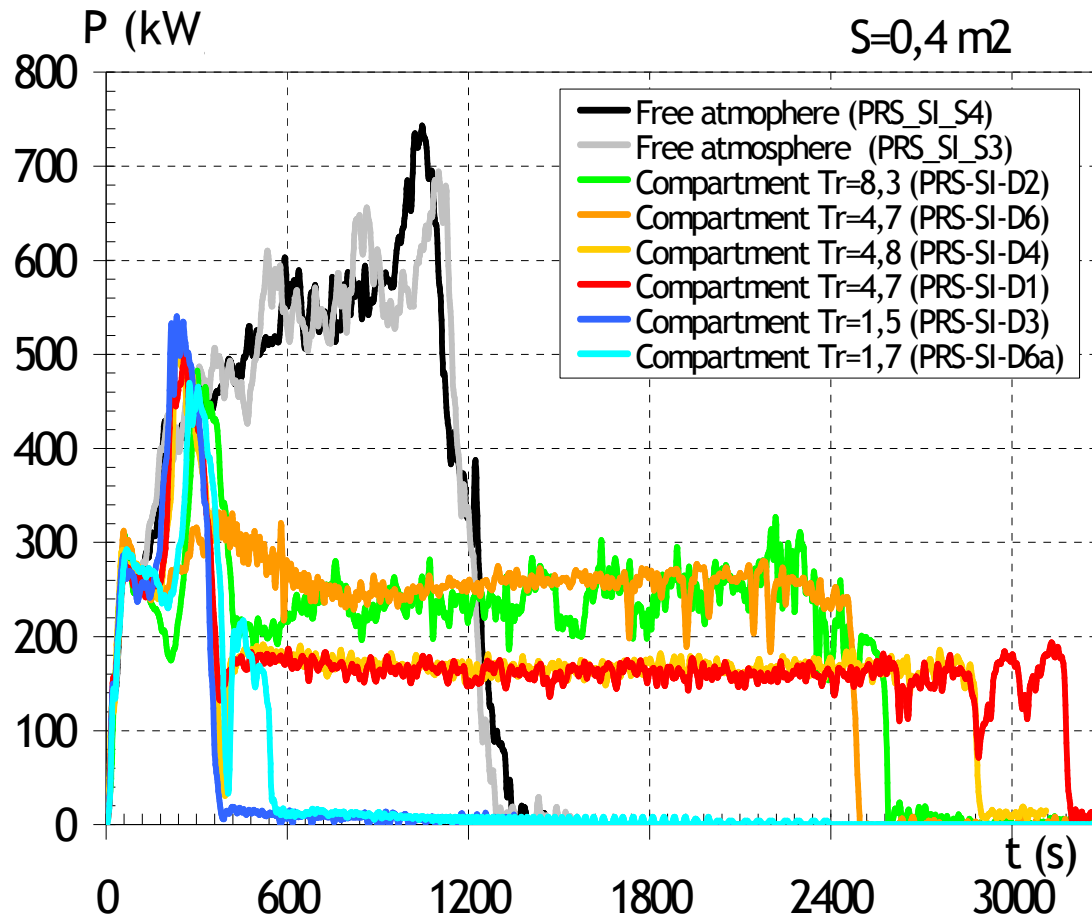
■ PRISME Source (2005 & 2007)

- around 20 tests in open atmosphere (SATURNE hood)
 - Various heat release rate
- 8 tests in confined atmosphere (DIVA Facility)
 - Large range of ventilation conditions (one room)
- Fuel: Dodecane (HTP)



Pretré, H., Querre, P., "Experimental Study of Burning Rate Behaviour in Confined and Ventilated Fire Compartments", 8th IAFSS, 2005, pp. 1217-1229.

Heat Release rate



Name	S (m ²)	Tr	Inlet Position
SI_D1	0.4	4.7	U
SI_D4			U
SI_D2		8.4	U
SI_D3		1.5	U
SI_D5	0.2	4.6	U
SI_D5a			1.6
SI_D6	0.4	4.7	L
SI_D6a		1.7	L

PRISME Program (2006-2010)

■ Propagation modes

- PRISME Door (2007 - 6 tests)
 - Propagation through a door
 - 2 or 3 rooms
 - Under and over ventilated conditions
- PRISME leak (2008 - 4 tests)
 - Propagation through leakages
 - Heat of a crossing ventilation duct

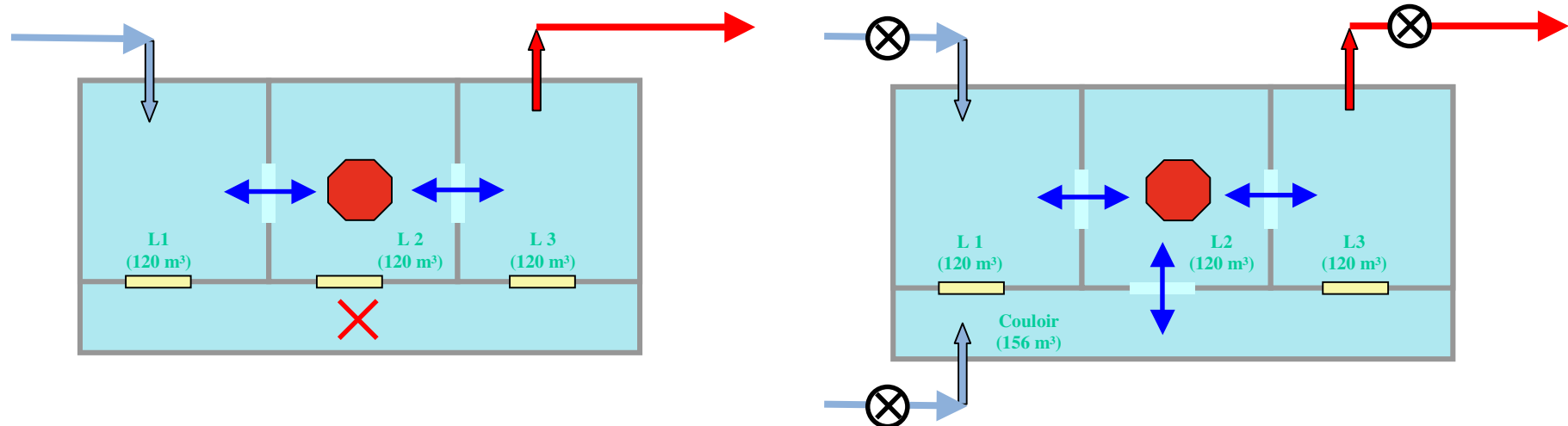
■ Real scenarios

- PRISME Integral (6 tests):
 - Specification: Discussions with partners underway
 - Realisation: 2010

PRISME Program (2006-2010)

■ PRISME Integral

- Only one parameter will change in order to compare tests among themselves
 - Test 1: 3 rooms, TPH
 - Test 2: 3 rooms, TPH, **sprinkler**
 - Test 3: 3 rooms, **real fire source: vertical cables tray**
 - Test 4: **4 rooms**, TPH.
 - Test 5: 4 rooms, TPH, **dampers**
 - Test 6: 4 rooms, **real fire source: electrical cabinet**, dampers.



Specifications of the 1st exercise

■ BE #1

- Post-calculations of the PRISME Source tests in the DIVA facility
- Pre-calculations of the PRISME Door tests

■ Objectives:

- to evaluate the fire codes capabilities to model
 - The effect of under-ventilation conditions on the burning rate
 - The interaction between fire and ventilation network
 - The smoke and soot propagation from the fire room to the adjacent room
 - The thermal stress on several targets located in the rooms

BE #1

■ Status of Numerical Results (Website / E-mail) (27th March 2009)

Type	Computer code	Organisation	PRS-SI-D1
CFD	FDS (v4)	CSN	○
CFD	FDS (v4)	JNES	○
CFD	FDS (v4)	IBMB	○
CFD	FDS (v4)	NRG	○
CFD	FDS (v4)	Tractebel	○
CFD	FDS (V5)	Lund University / Vattenfall	PBG 7
CFD	FDS (v5, Dev)	VTT	○
CFD	FDS (v5)	KINS	○
CFD	SAFIR	Université de Provence / DGA	PBG 7
CFD	ISIS (v1.0, Dev)	IRSN	○
Lumped	COCOSYS (v2.4, Dev)	GRS	○
Zones	CFAST (v5.0)	JNES	○
Zones	CFAST	BEL V	○
Zones	CFAST (v6.0)	NRG	○
Zones	CEIL (v1.5)	DGA	○
Zones	MAGIC (v4.1.2)	EDF	○
Zones	SYLVIA (v1.2.2, Dev)	IRSN	○

17 Participants

8 codes used

BE #1

■ Initial proposal

Name	Nber of Rooms	Pool Surface	Renewal rate	Inlet location
PRS_SI_D1	1	0.4 m ²	4.7 h ⁻¹ (560 m ³ h ⁻¹)	High
PRS_SI_D3	1	0.4 m ²	1.5 h ⁻¹ (180 m ³ h ⁻¹)	High
PRS_SI_D6	1	0.4 m ²	4.7 h ⁻¹ (560 m ³ h ⁻¹)	Low
PRS_D1 (Door)	2	0.4 m ²	0 h ⁻¹ (0 m ³ h ⁻¹)	High
PRS_D3 (Door)	2	0.4 m ²	4.7 h ⁻¹ (180 m ³ h ⁻¹)	High

 : Open calculations

 : Blind calculations

■ Final proposal

- PRS SOURCE D1 with experimental HRR as input data
- Discussion on the metrics

BE #1

L2-Norm Index (Peacock):

$$\frac{\|\Delta \vec{Y}\|}{\|\vec{Y}_{\text{exp}}\|} = \frac{\|\vec{Y}_{\text{exp}} - \vec{Y}_{\text{num}}\|}{\|\vec{Y}_{\text{exp}}\|} = \frac{\sqrt{\sum_i (Y_{\text{exp},i} - Y_{\text{num},i})^2}}{\sqrt{\sum_i (Y_{\text{exp},i})^2}}$$

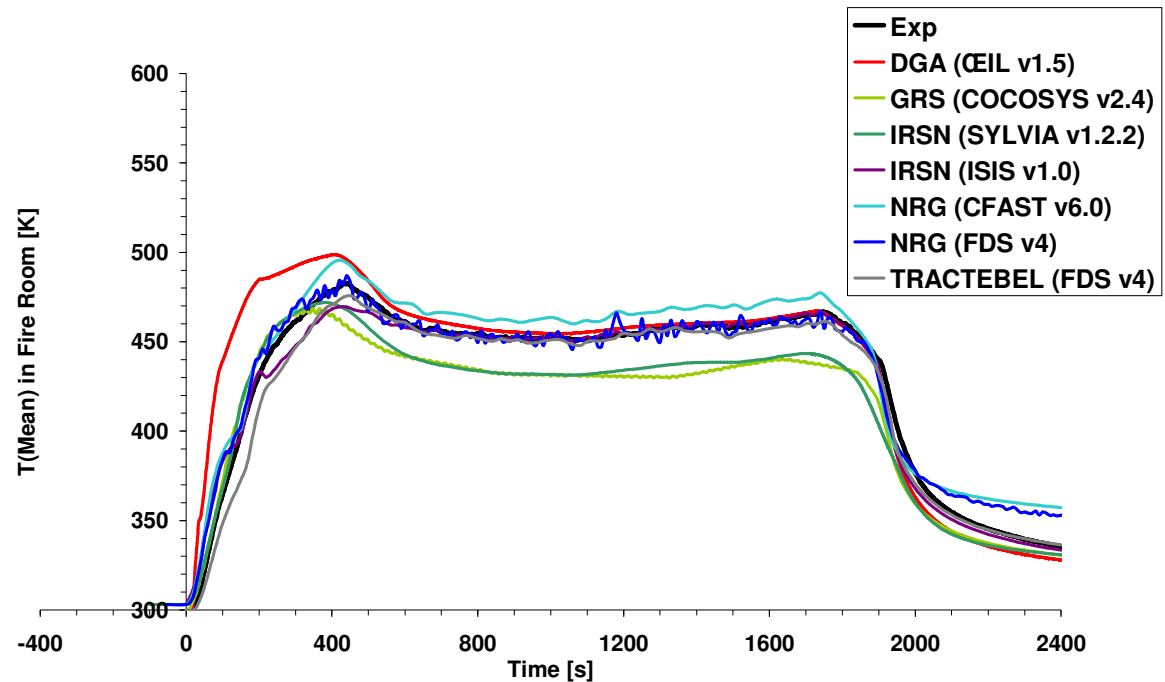
Type: Global ; **Bounded:** No ($[0; +\infty[$) ; **Success:** $|I| \approx 0$

Meaning (Peacock-99):

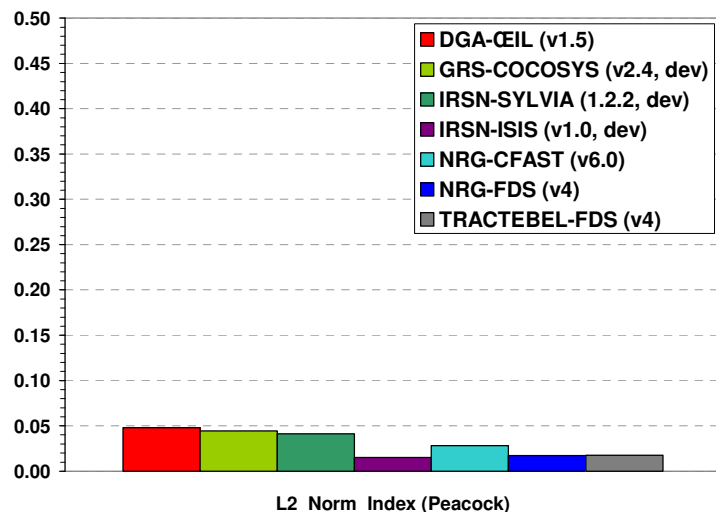
“This norm based upon relative difference provides a measure of the difference in overall magnitude for the two curves (exp/num) normalized to the experimental data.”

BE #1

Mean temperature in fire room



Mean Temperature in Fire Room

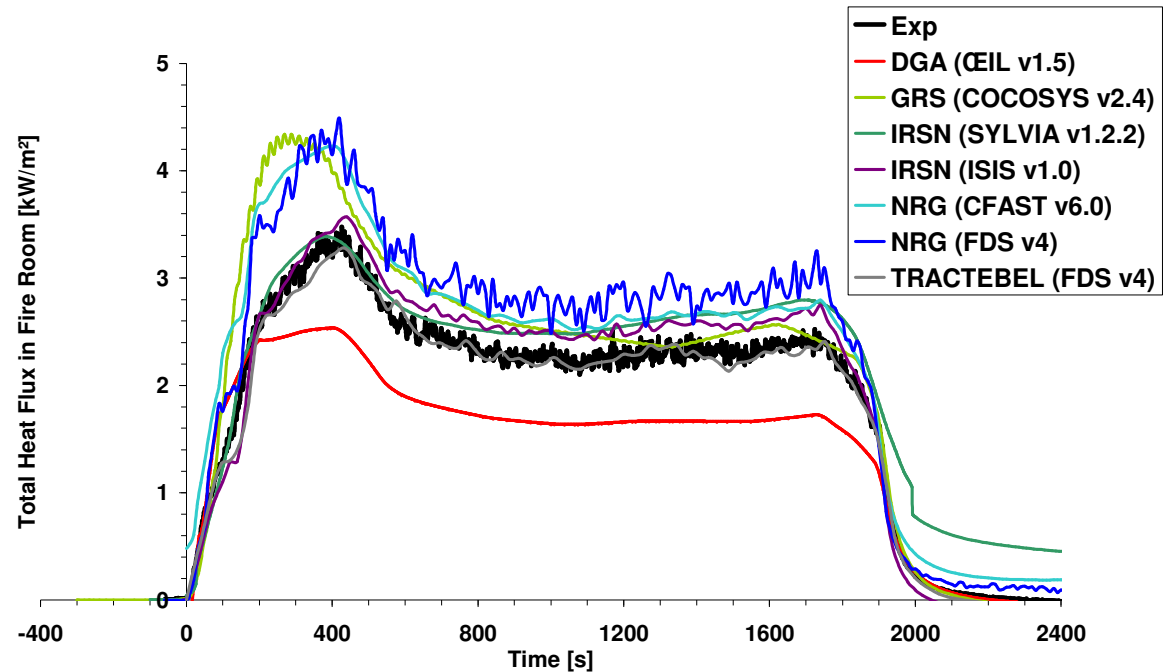


Comments:

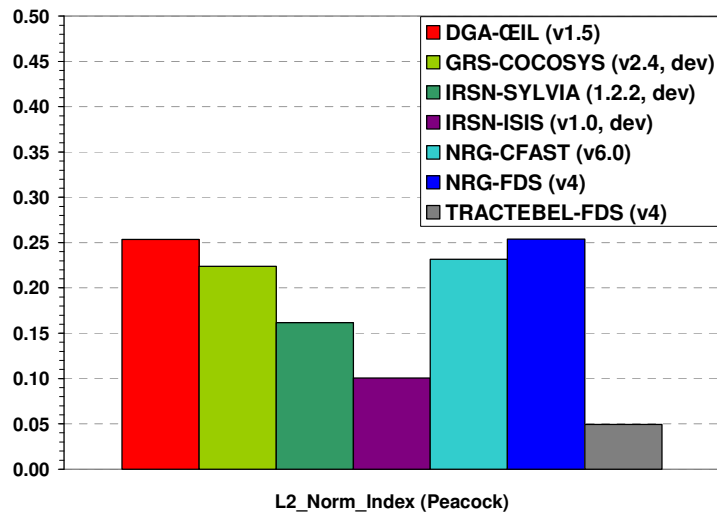
- All results are in good agreement.
- COCOSYS and SYLVIA are very close and slightly lower than the others codes and exp. data.
- The L2-norms give low values (<0.05) => good results.

BE #1

Total heat flux to the north wall in fire room



Total Heat Flux (mid-height) in Fire Room



Comments:

- Three codes (COCOSYS, CFAST, FDS-NRG) are above the exp. data.
- One code (OEIL) is below the exp. data.
- Three codes (SYLVIA, ISIS, FDS-TRACTEBEL) are in good agreement with the exp. Data.
- The L2-norms confirms this conclusion.

BE #1

■ Application of the metrics

- Comparisons with experimental data
 - Mean Gas temperature
 - Gas pressure
 - Vent flow (ISIS, MAGIC, COCOSYS, OEIL, SAFIR)
 - Heat Fluxes at 2.6 m
 - Oxygen concentration
 - Wall temperature at 2.6 m

- Relevant metrics according the fire phase
 - Ignition
 - Stationary phase
 - Extinction

■ Publication in progress

BE #2

■ Sensitive Analysis

- Fire test: Same test proposed in BE #1
 - PRS-SI-D1 ($S=0.4 \text{ m}^2$; TPH ; 4.7 RR)
- Input parameters

Heat of combustion

	Input parameters	Init. Value	Lower value	Upper value	Reference
Fuel	HRP [kW] (1)	Q(t)	-10%	+10%	PRISME-27
Fuel	X_r [-]	0.35	0.3	0.4	PRISME-23
Wall (concrete)	k [W/m/K] (2)	1.5	1.07	1.93	PRISME-09
Wall (concrete)	Cp [J/kg/K] (3)	740	280	1200	PRISME-09
Wall (concrete)	\square [-]	0.7	0.5	0.9	BE
Ventilation	Q_v [m ³ /h]	560	500 (-10%)	620 (+10%)	PRISME-27

1000 J/kg/K 800 J/kg/K

BE #2

- **Partners Simulations (March 2009)**
 - Monte-Carlo Simulations
 - FDS (VTT)
 - COCOSYS (GRS)
 - Fractional Factorial Design
 - FDS (KINS)
 - MAGIC (EDF)
 - SYLVIA (IRSN)

- **Comparison of the two approaches**
 - FDS (VTT)
 - COCOSYS (GRS)
 - SYLVIA (IRSN)

BE #2

■ Outputs analysis

- Mean temperature
 - Maximum value
 - At a given time during the steady phase: at $t = 2000$ s
- Minimum oxygen mass fraction
 - Upper layer for zones codes
 - At $z = 3$ m for CFD codes
- maximum wall temperature at 2.6 m
- maximum radiative heat flux at 2.6 m
- Total heat fluxes at 2.6 m
- (Pressure)
 - At a given time during the steady phase: at $t = 2000$ s
 - maximum value (overpressure)
 - minimum value (under pressure)