Large-Eddy simulation of a certification burner with fully coupled conjugate heat transfer

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Projet PRC AETHER DGAC

Journée GdR Feux/GFC, 6/7 décembre 2018









Motivation

Context

- Manufacturers need to certify equipment in terms of fire resistance (housing, fastening engine, ...)
- Certification: the apparatus needs to be submitted [1]
 - to a kerosene / air burner
 - during a fixed time (5 to 15 minutes)
 - with a standardized flame: 1100°C (\approx 1300K) and 116 kW/m²

Objective

- Model fire resistance tests with Large-Eddy Simulation
- Improve comprehension of phenomena involved in tests
- Try to minimize the risk in the real certification tests
- Difficulties
 - Very different time and space scales
 - Multi-physics and complex geometry
 - Very few studies



Liquid-fuel burner





Large-Eddy Simulation in the aeronautical context

- LES is well suited to the high-fidelity simulation of aeronautical burners
- Challenges
 - Unsteady, multi-scale, multi-physics flows
 - Need to exploit modern super-computers



Aircraft engine chamber



JOLIOT-CURIE, PRACE/GENCI at the Très Grand Centre de Calcul, CEA P9 Petaflops, 124 000 cores



The CFD platform: YALES2

- Developed by CORIA and the French Combustion Community +250 researchers/engineers trained at CORIA since 2009 +110 articles (Google Scholar)
- A unique network to ease collaboration and transfer of numerics and models to the industry



CNRS – UNIVERSITE et INSA de Rouen

The CFD platform: YALES2

- Features
 - Unstructured meshes (complex geometries) and adaptive grid refinement
 - Low-Mach number Navier-Stokes equations (incompressible and variable density) solved with a projection method
 - Double-domain decomposition [3]
 - Highly efficient solvers for linear system inversion (PCG, DPCG)
 - 4th-order central finite-volume method and 4th-order time integration
 - Two-phase flows (Lagrangian particles)
 - Spray and atomization (Levelset)
 - Combustion modeling (Tabulated or complex chemistry, NOx prediction model...)
 - Suited for massively parallel computing (>32 000 procs)





YALES2 web site, <u>http://www.coria-cfd.fr</u>
 SUCCESS web site, <u>http://success.coria-cfd.fr</u>

Prediction of pollutant emissions in realistic burners: Application to a low-NOx helicopter engine

- LES from J. Lamouroux, SAFRAN Helicopter Engines, in 2015
- 376M elements for 2 injectors, tabulated chemistry, dedicated NOx model [1]



Prediction of pollutant emissions in realistic burners: Investigation of CO prediction

 PRACE project « FIRELES » (2018): LES of the lean-premixed PRECCINSTA burner with finite-rate chemistry (17 species, 73 reactions) and heat loss [1]



Prediction of pollutant emissions in realistic burners: Investigation of CO prediction

- PRACE project « FIRELES » (2018): LES of the lean-premixed PRECCINSTA burner with finite-rate chemistry (17 species, 73 reactions) and heat loss [1]
- Strong sensitivity of the CO prediction to mesh resolution



		Mesh	NAD1	NAD2	NAD3	NAD4
		Cell count [millions]	1.7	14	110	877
[1] P. Bénard et al. (2018) Int. Comb. Symp., Dublin		Cell size [mm]	1.2	0.6	0.3	0.15

The next step: towards dynamic mesh adaptation of massive meshes for front/interface capturing

- Collaboration of CORIA/INRIA/SAFRAN awarded at the TERATEC 2018 forum
- Objectives: reduction of CPU cost and modeling errors



[1] P. Bénard et al. (2016) Int. J. Num. Methods Fluids 81(12)
[2] C. Dobrzynski, P. Frey, (2018) 17th international Meshing Roundtable, USA.

The next step: towards dynamic mesh adaptation of massive meshes for front/interface capturing

- Collaboration with R. Mercier, J. Leparoux, H. Musaefendic, SAFRAN
- Strategy: conservative interface capturing [1] and mesh adaptation
- Objective: reproduce the jet penetration and granulometry



Kerosene jet-in-cross-flow at 10 bar [2]



$$We_{aero} = \frac{\rho_g V_g^2 D_{inj}}{\sigma} = 406.2$$
$$q = \frac{\rho_l V_l^2}{\rho_g V_g^2} = 49.6$$

Resolution of 10 microns at interface Up to 600 million cells Up to 10 000 cores (Xeon Broadwell)

Torch modeling strategy

- Multi-physics Spray Evaporation Flame
- Heat transfers
 Convection
 Conduction
 Radiation
- Numerical parameters
 - Finite-rate chemistry for kerosene:

Turbulator

Injection line

- 2-steps scheme (BFER) [1]
- Liquid & gas injection:
 - Lagrangian spray model
 - adjusted thanks to exp. Data
- No soot model (noticeable limitation)
- Characteristic numbers
 - Phi = 0.77, Reynolds = 30 700

Cone

Torch modeling strategy: couplings

• Coupling of different solvers





Radiative heat transfer solver

- Discrete Ordinate Method
- Full spectrum SNB-CK model with EM2C database [1,2,3,4]
- Includes CO2, H2O, CO & CH4
- No SGS Turbulent-Radiation Interaction
- Quadrature methods
 - Gauss-Lobato (7pts and 20pts)
 - Gauss-Legendre (2pts, 4pts and 7pts)
 - Gauss-Radau [5] (7pts)
- In 2D: S4 (2 directions/quadrant) to S32 (16 directions/quadrant)
- In 3D: S4 (3 directions/octant) to S8 (6 directions/octant)
- 4th-order central FV scheme with 10% upwind for the RTE [6]
- High-Performance Computing
 - Simultaneous solving of all equations (BiCGStab(2) solver)
 - Optimized Brent Method to solve for k* for each spectral quadrature point
 - Fully vectorized



[4] Rivière & Soufiani (2012). Int. J. Heat Mass Transfer[5] Rivière (1992). J. Quant. Spectro. & Radiative Transfer[6] Nguyen (2010). ECCOMAS CFD2010







1/8 of space

Performances of radiative solver





CHT strategy: variables & solver interactions

- CHT coupling must be performed on a • parallel super-computer
- 2 strategies •
 - Sequential coupling
 - Asynchronous coupling



Solvers compute simultaneously 🖬 time saved

Solvers compute successively ime wasted

 ϕ_n



Solid Need: $\phi_{\mathrm{n-1}}$

> Solid Need: ϕ_n

> > [1] http://www.cerfacs.fr/globc/PALM WEB/ [2] F. Duchaine (2009). Int Journal of Heat & Fluid Flow

Fluid

Need: T_n

Fluid

[3] A. Felippa (2001). Comput. methods in appl mech & eng

Validation: INTRIG burner

1] Miguel-Brebion (2016). Comb & Flame 2] Xavier (2017). JFM 3] Meija (2017). Proceedings Comb Inst 4] Meija (2018). Comb & Flame

- INTRIG burner [1,2,3,4]
 - Laminar premixed flame anchored to a steel cylinder
 - Mixture: CH₄ and Air
- Heat transfer
 - Fully coupled CHT/RTE with participative medium
- Numerical parameters
 - Fluid: air at $u \approx 1 m/s$
 - Re = 584
 - Von-Karman streets at 40Hz
 - 2D Mesh: 630 000 tetrahedrons
 - $70\mu m$ in flame and solid
 - Prisms of $20\mu m$ at interface

Part to simulate







Validation: INTRIG burner

- 2 types of flame stabilisation
 - $\varepsilon = 1.0$: downstream stabilized
 - Low T & little recirculation zone
 - $\varepsilon = 0.0$: upstream stabilized
 - High T & large recirculation zone
- Angle profile
 - Gap between arepsilon=0.15 and arepsilon=0.1
 - Good comparison with Miguel-Brebion (2016). Comb & Flame







Certification torch: Numerical setup



Turbulator:



Front



Simulation domain $\approx 3m^3$



- Fluid:
 - From 0.4 to 2 mm
 - Cell count: 40M tets
 - Max y+ around 4 inside
- Solid:
 - From 0.2 to 1 mm
 - Cell count: 140M tets
 thinness of the cone





Topology of the flame: adiabatic case

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- **Corner recirculation zone**
- **High values of fuel** consumption where the flame is the strongest
- Large-scale flame wrinkling due to the turbulator
- Individual droplet evaporation at the wall and group droplet evaporation in the center
- Gaseous kerosene found at the wall due to large droplets crossing the flame

Flow













Topology of the flow inside and outside

- Rendering of high values of $\dot{\omega}_T$ during 20ms
 - Wrinkling due to the turbulator
 - Isolated hot spots: combustion of droplets





- Fluid: 1024 cores / Solid: 60 cores
- 6h on Occigen, CINES
- Upper side: buoyancy driven flow ($R_a = 6.10^6$)
- Lower side: stable stratification

Rendering of T in the air

Topology of the flame: adiabatic vs CHT

- Droplet evaporation starts upstream of the flame
- w/ CHT: consumption at the wall & the outlet
- w/ CHT: presence of gaseous kerosene on the walls Flame lift-off more important w/o CHT: Hotter recirculation zones
- Large-scale flame wrinkling unaffected by CHT
- Hot air plume above the cone





Temperature profiles

- Instantaneous temperature fields
 - Seems to be lower with participative gases
- Mean temperature at the outlet
 - Adiabatic: too high values
 - Transparent: same level as adiab. case
 - Participative: $\approx 200 K$ lower -> almost at ISO values
 - Limitations
 - Simple chemistry (2 reactions)
 - No model for soot formation/radiation





Т

External wall temperatures

	Expérimental	Milieu transparent	Milieu participatif
Température [°C] ++			

Conclusion & perspectives

- LES of certification burners is challenging but feasible
 - Long integration time / large domain volume
 - Multi-physics
- Many models and sub-models are still required in this work
 - Soot formation/radiation models
 - More detailed chemistry for kerosene
- Perspectives
 - Comparison of T & *φ* on plane plate with exp. results
 - Simulation of a real certification test with engine envelope



